Moment Integrations for 3D Printed Shapes



Nobuyuki Umetani Autodesk Research



Overview

- Intro
- Integration over 3D domain
- Mass
- Center of Mass
- Moment of Inertia

Inhomogeneous Material Distribution

color



http://www.stratasys.com/

stiffness



[Skouras et al.2013]

Inhomogeneous Density Distribution



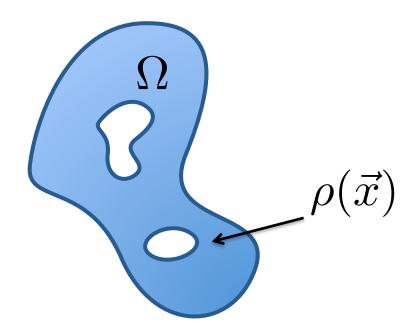


Built-to-last, [Lu et al. 2014]

Buoyancy Optimization, [Wang et al. 2016]

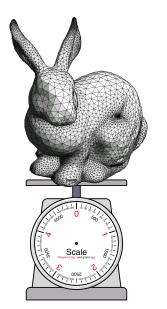
Measure of 3D Density Distribution

 How much density information can you still measure without seeing 'inside' of a 3D shape?

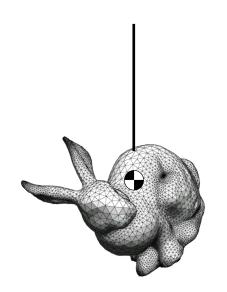


Invariants of 3D Density Distribution

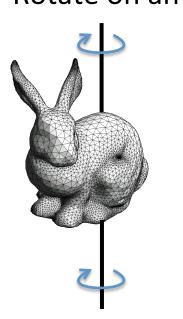
Put on the scale



Hang on a string



Rotate on an axis

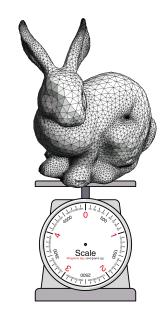


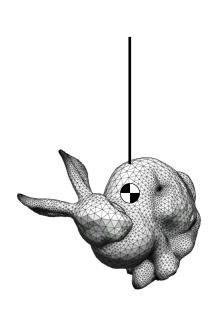
Invariants of 3D Density Distribution

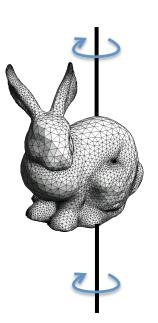
Mass

Center of Mass

Moment of Inertia







Invariants of 3D Density Distribution

Mass

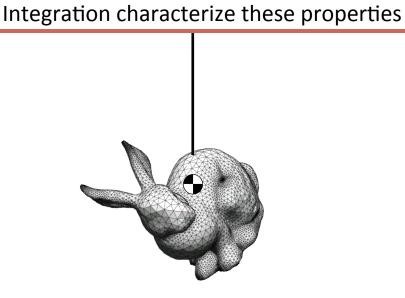
Center of Mass

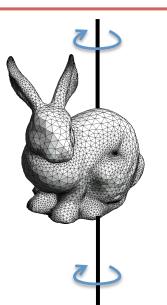
Moment of Inertia

$$\int_{\Omega} (\vec{x})^0 dv$$

$$\int_{\Omega} (\vec{x})^1 dv$$

 $\int_{\Omega} (\vec{x})^2 dt$



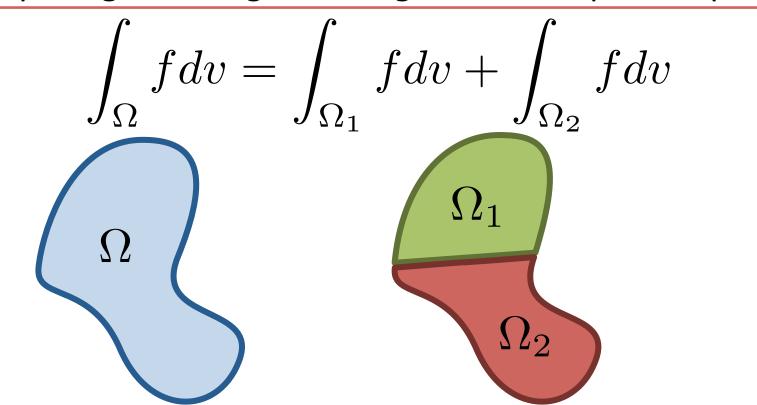


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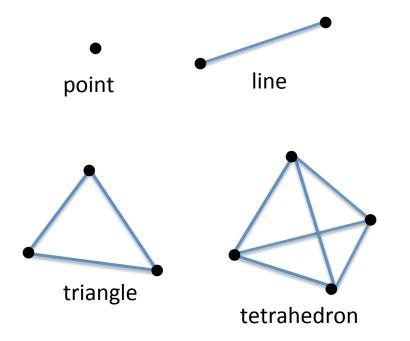
Integration Formula is Convenient

Decomposing the integration region into simpler shapes



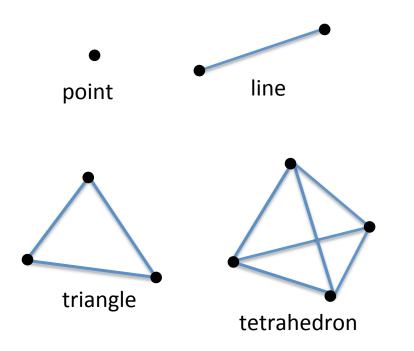
Integration Rules for the Simplex Shape

Simplex shape

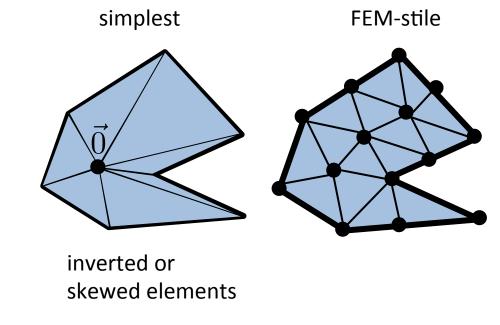


Integration Rules for the Simplex Shape

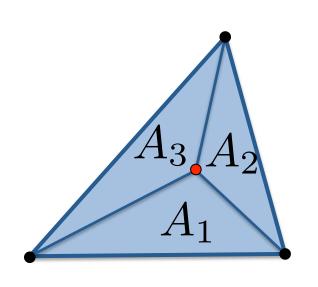
Simplex shape



Decomposition



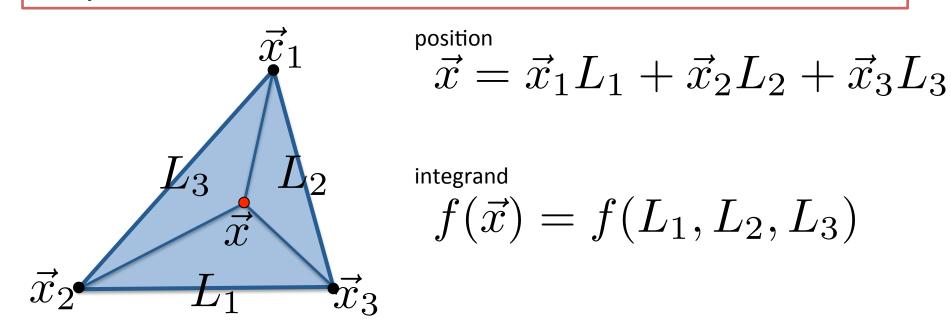
Barycentric coordinate (L_1, L_2, L_3)



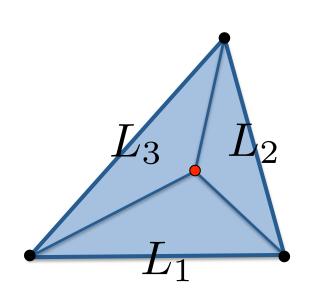
$$A = A_1 + A_2 + A_3$$

$$L_i = A_i/A$$

Position and integrand are both represented using the Barycentric coordinate



For polynomial integrands, there is an analytic integration formula



$$f(L_1, L_2, L_3) = L_1^a L_2^b L_3^c$$



Integration over the triangle

$$\int_{A} L_{1}^{a} L_{2}^{b} L_{3}^{c} da = \frac{a!b!c!2!}{(a+b+c+2)!} A$$

$$\int_{L} L_{1}^{a} L_{2}^{b} dl = \frac{a!b!1!}{(a+b+1)!} L$$

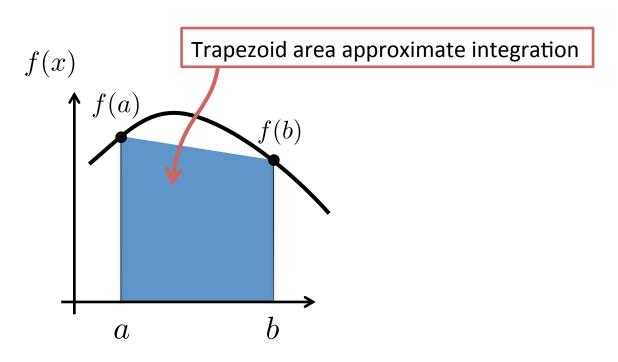
$$\int_{A} L_{1}^{a} L_{2}^{b} L_{3}^{c} da = \frac{a!b!c!2!}{(a+b+c+2)!} A$$

$$\int_{V} L_{1}^{a} L_{2}^{b} L_{3}^{c} L_{4}^{d} dv = \frac{a!b!c!d!3!}{(a+b+c+d+3)!} V$$

Proof of them is VERY difficult (need the Gamma function) https://en.wikipedia.org/wiki/Beta_function

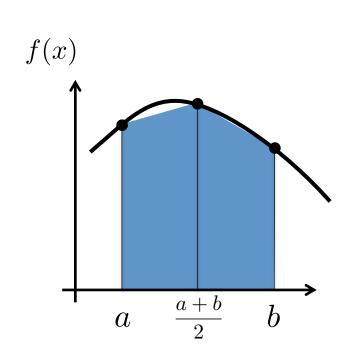
Integration Rules: Numerical

Trapezoid rule

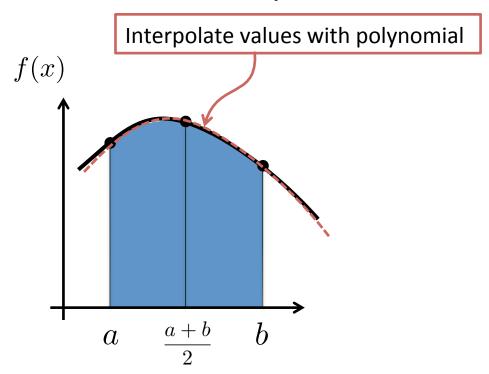


Integration Rules: Numerical

Trapezoid rule

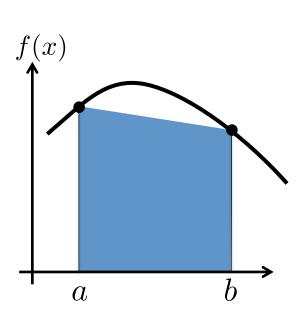


Newton-Cotes quadrature

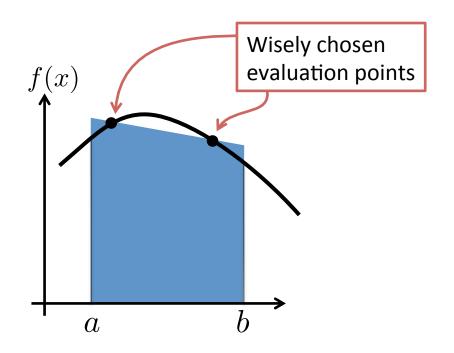


Integration Rules: Numerical

Trapezoid rule



Gauss quadrature



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Mass

$$M = \sum_{i=1}^{n} m_i \qquad m_1 \qquad m_3$$

Mass

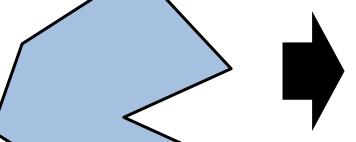
$$M = \sum_{i=1}^{\infty} m_i \qquad \underbrace{m_1}_{m_3}$$

$$M = \int_{V} \rho(\vec{x}) dV \qquad \longrightarrow \qquad M = \rho \int_{V} dV$$

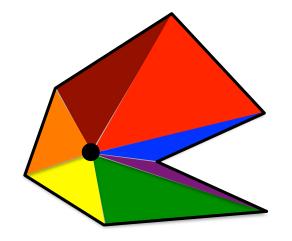
Homogeneous

Computing volume integral using volume discretization

Volume integral



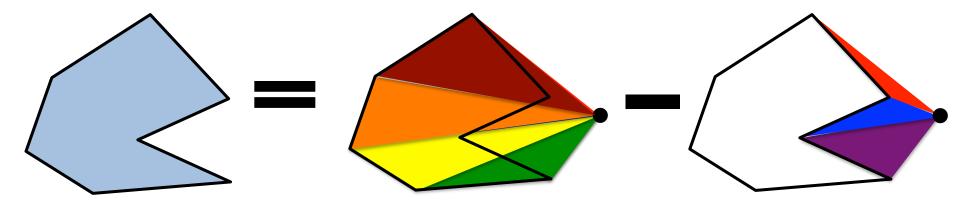
Divide the region into simplexes



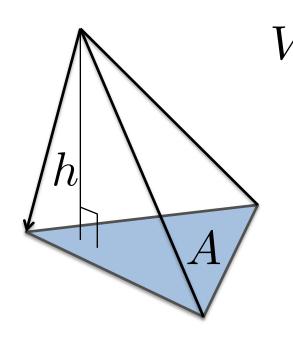
Computing volume integral using volume discretization

Volume integral

OK to be inverted. The area can be minus

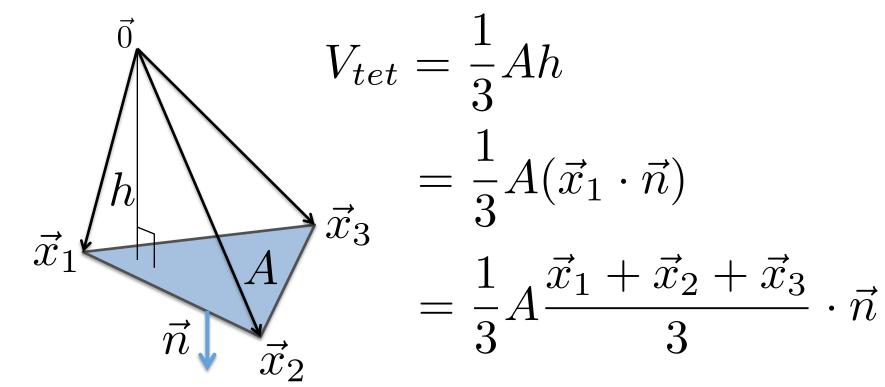


Volume of a tetrahedron

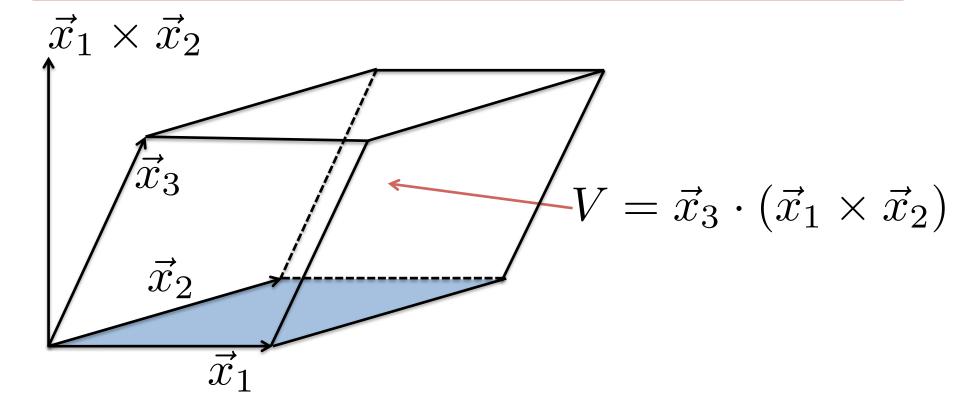


$$V_{tet} = \frac{1}{3}Ah$$

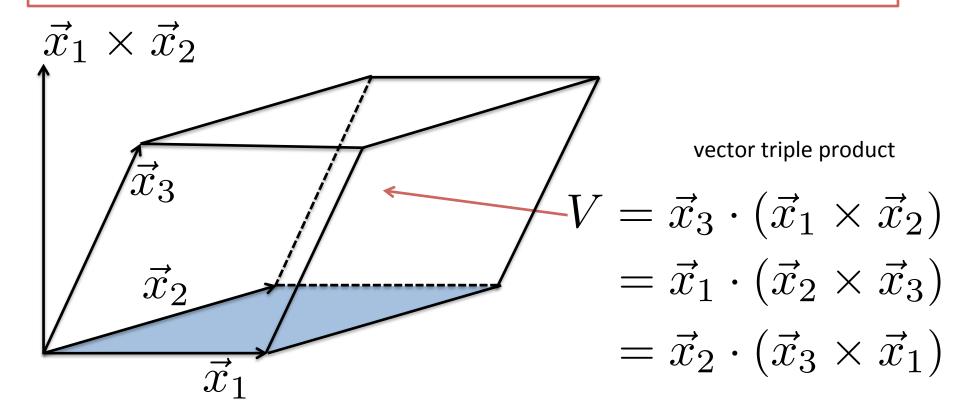
Volume of a tetrahedron



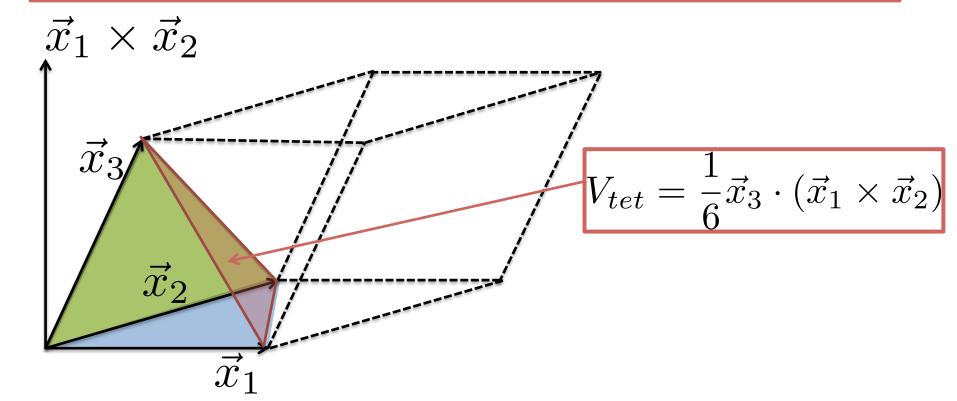
Volume of a tetrahedron can be computed from a parallelepiped



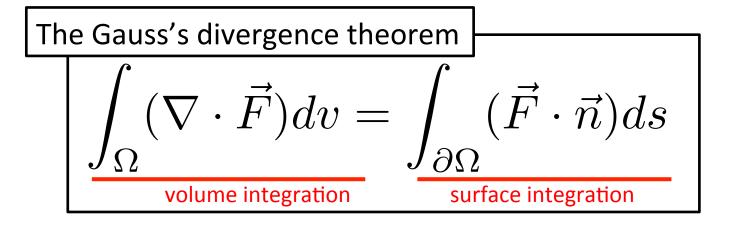
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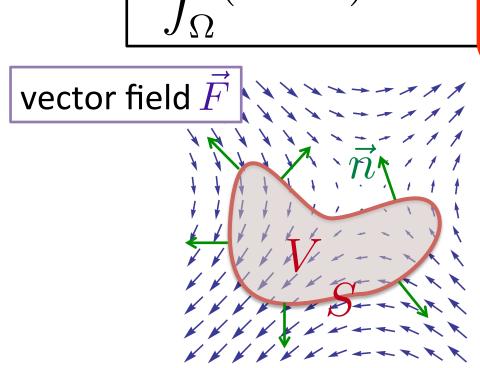
Volume of a tetrahedron can be computed from a parallelepiped



Computing volume integration using surface integration



$$\int_{\Omega} (\nabla \cdot \vec{F}) dv = \int_{\partial \Omega} (\vec{F} \cdot \vec{n}) ds$$



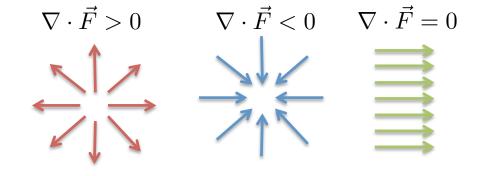
measures total outward flow through V's boundary

add up little bits of outward flow in V

$$\int_{\Omega} (\nabla \cdot \vec{F}) dv = \int_{\partial \Omega} (\vec{F} \cdot \vec{n}) ds$$

divergence

$$= \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z}$$



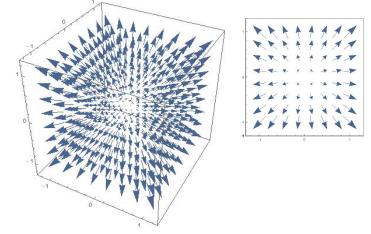
$$\int_{\Omega} dv = \int_{\Omega} (\nabla \cdot \vec{F}) dv = \int_{\partial \Omega} (\vec{F} \cdot \vec{n}) ds$$

$$\nabla \cdot \vec{F} = 1$$

 $abla \cdot \vec{F} = 1$ What's the \vec{F} looks like?

One example for $ec{F}$

$$\vec{F} = \frac{1}{3}\vec{x} = \frac{1}{3}(x\vec{e}_x + y\vec{e}_y + z\vec{e}_z)$$

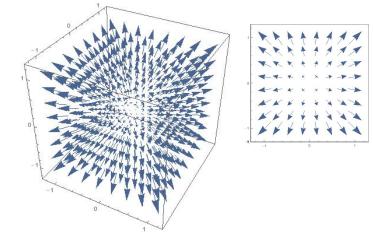




$$\int_{\Omega} dv = \int_{\partial \Omega} \left(\frac{1}{3} \vec{x} \cdot \vec{n} \right) ds = \sum_{t \in T_{ri}} \int_{\partial \Omega_t} \left(\frac{1}{3} \vec{x} \cdot \vec{n} \right) ds$$

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$$\vec{F} = \frac{1}{3}\vec{x} = \frac{1}{3}(x\vec{e}_x + y\vec{e}_y + z\vec{e}_z)$$

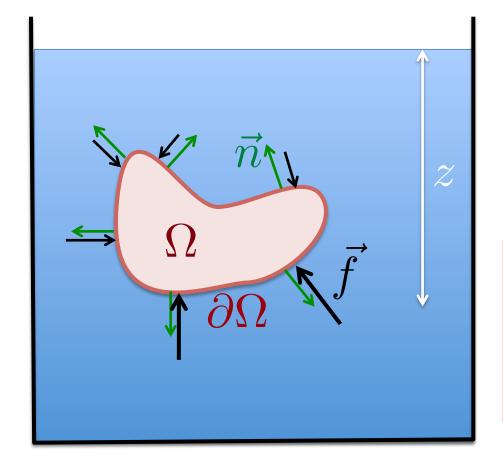




$$\int_{\Omega} dv = \int_{\partial \Omega} \left(\frac{1}{3} \vec{x} \cdot \vec{n} \right) ds = \sum_{t \in T_{ri}} \int_{\partial \Omega_t} \left(\frac{1}{3} \vec{x} \cdot \vec{n} \right) ds$$

$$\int_{\partial\Omega_t} \frac{1}{3} (L_1 \vec{x}_1 + L_2 \vec{x}_2 + L_3 \vec{x}_3) \cdot \vec{n} ds = \frac{1}{3} A \frac{\vec{x}_1 + \vec{x}_2 + \vec{x}_3}{3} \cdot \vec{n}$$

Application of Mass: Buoyancy



Force on the surface is always in normal direction

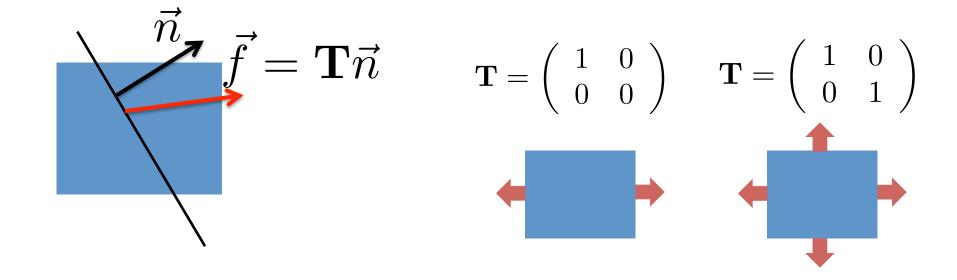
$$\vec{f} = -\rho g z \vec{n}$$

$$= \vec{T} \vec{n}$$

Cauchy stress
$$T = -\rho g \left(\begin{array}{ccc} z & 0 & 0 \\ 0 & z & 0 \\ 0 & 0 & z \end{array} \right)$$

Cauchy Stress Tensor

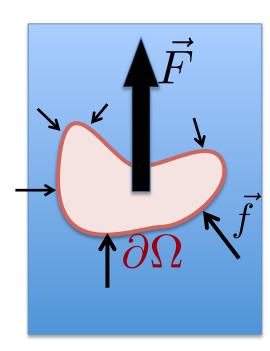
Symmetric matrix that relate cutting plane normal \vec{n} and force on the cutting plane \vec{f}



Application of Mass: Buoyancy

We can now proof Archimedes' principle.

$$\vec{F} = \int_{\partial\Omega} \vec{f} ds = \int_{\partial\Omega} (\mathbf{T} \cdot \vec{n}) ds = ?$$



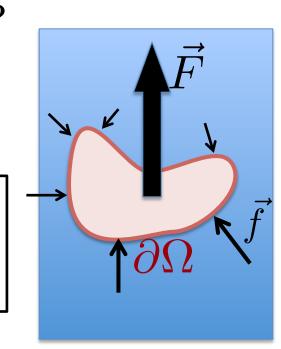
Application of Mass: Buoyancy

We can now proof Archimedes' principle.

$$\vec{F} = \int_{\partial \Omega} \vec{f} ds = \int_{\partial \Omega} (\mathbf{T} \cdot \vec{n}) ds = ?$$

The divergence theorem for tensor

$$\int_{\Omega} (\nabla \cdot \mathbf{T}) dv = \int_{\partial \Omega} (\mathbf{T} \cdot \vec{n}) ds$$



Interesting Object: Cartesian Diver





https://www.youtube.com/watch?v=sNOXFiJ4IDU

Research in CG: Buoyancy Optimization

Buoyancy Optimization for Computational Fabrication

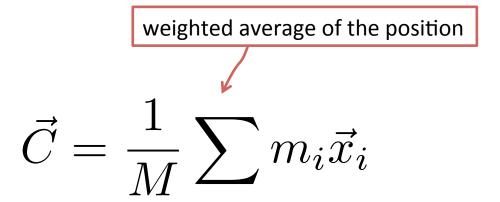
Lingfeng Wang Emily Whiting

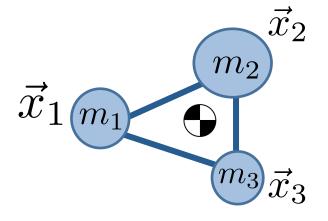
Dartmouth College, USA

Overview

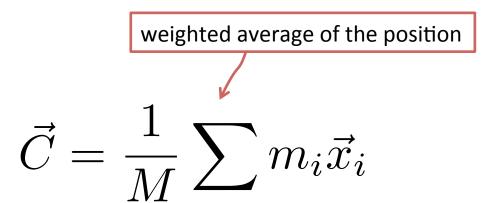
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- Integration over 3D domain
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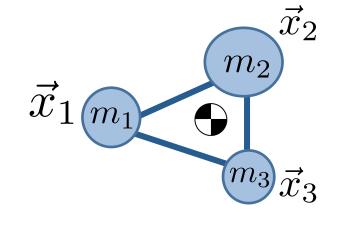
The Center of Mass





The Center of Mass



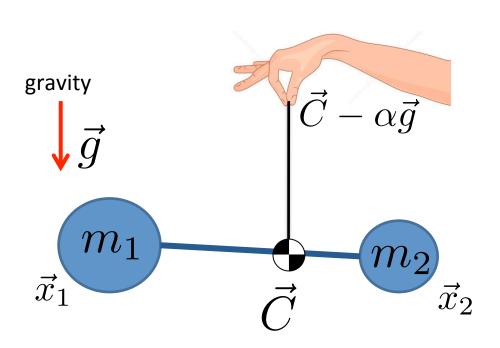


$$\vec{C} = \frac{1}{M} \int_{\Omega} \rho(\vec{x}) \vec{x} dv \xrightarrow{\text{density}} \vec{C} = \frac{\rho}{M} \int_{\Omega} \vec{x} dv$$

Homogeneous

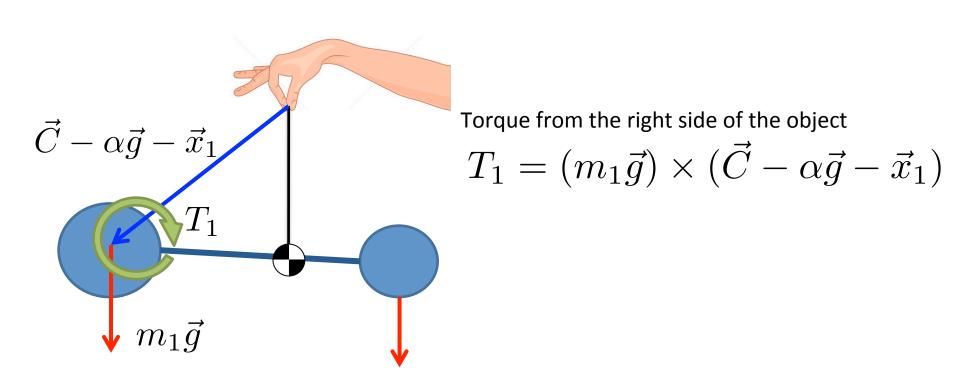
The Center of Mass and Balance

We can hang an object static by putting string above CM



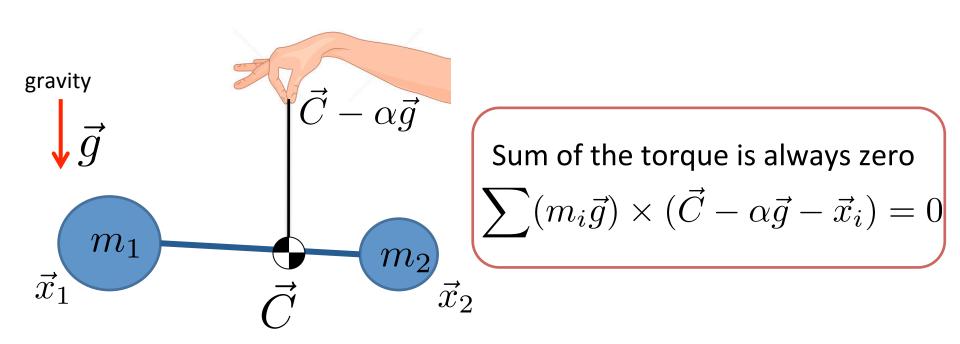
The Center of Mass and Balance

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The Center of Mass and Balance

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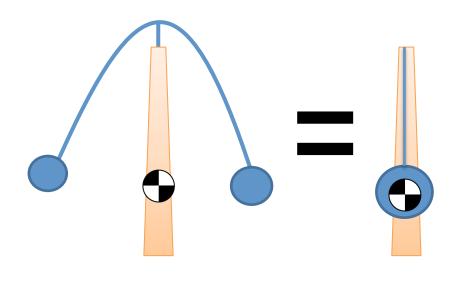
Balancing Toy



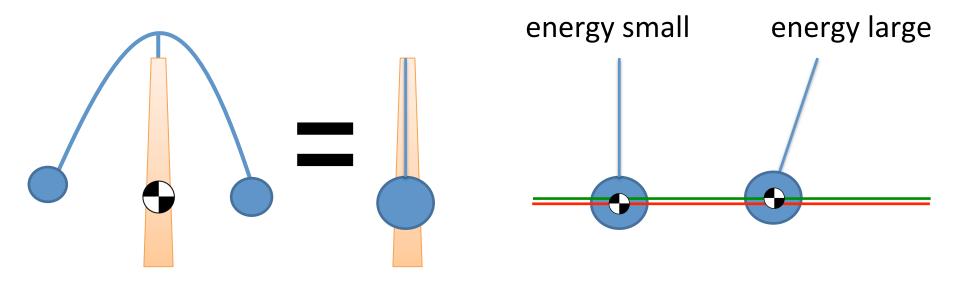


https://www.youtube.com/watch?v=wKvk-Q7U3nM

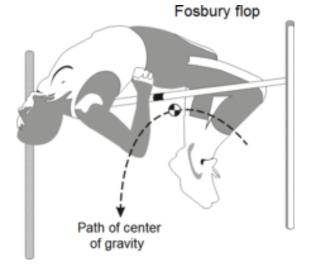
Criteria for Stability: Point Support



Criteria for Stability: Point Support



CM Can be Outside: The Fosbury Flop





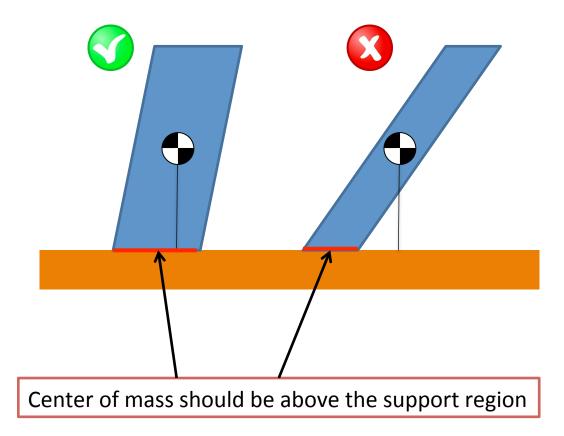
[TED Ed, https://www.youtube.com/watch?v=RaGUW1d0w8g]

1968 summer Olympic in Mexico City

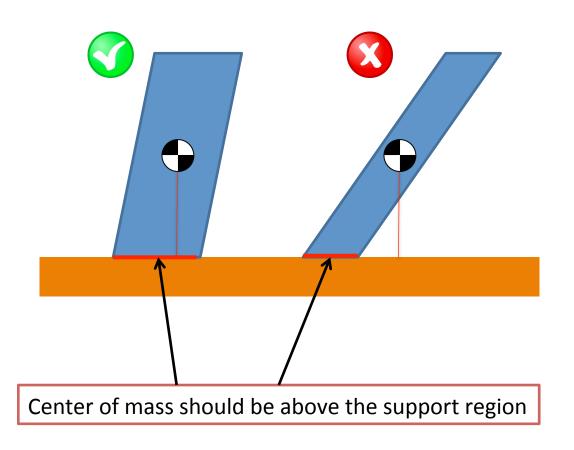


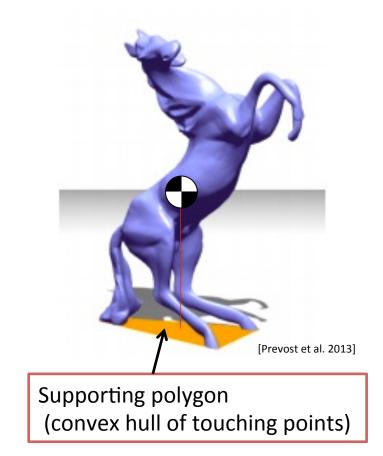
https://www.youtube.com/watch?v=Id4W6VA0uLc

Criteria for Stability: Standing



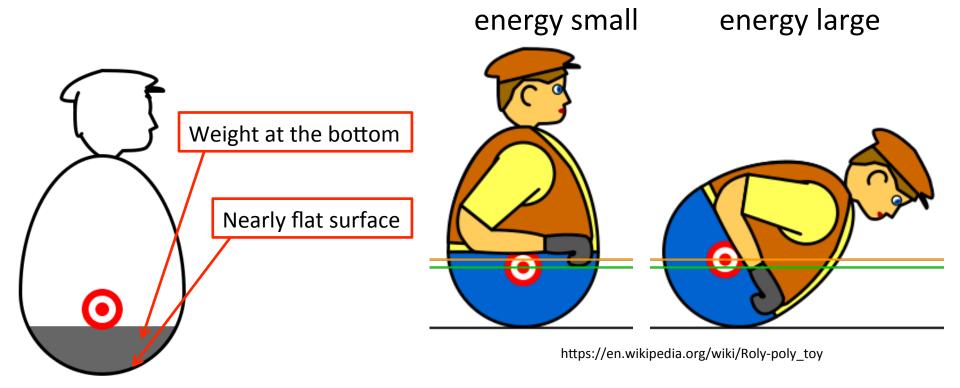
Criteria for Stability: Standing



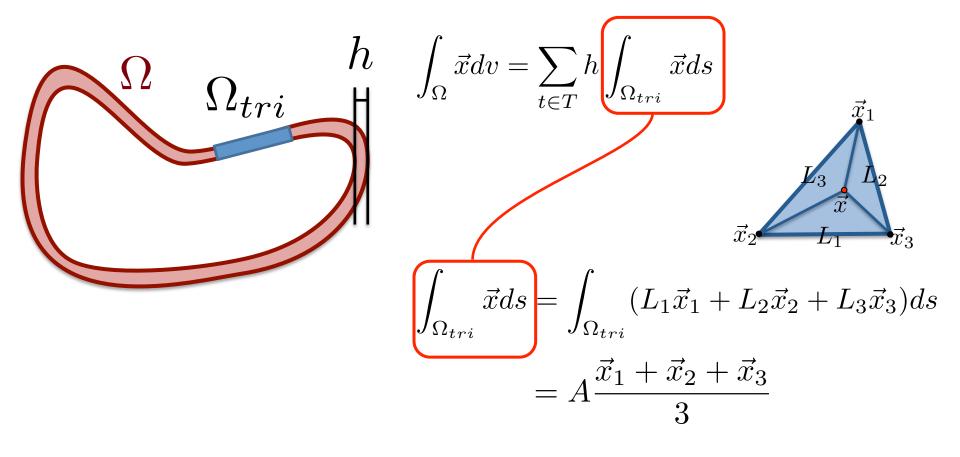


Criteria for Stability: Smooth Surface

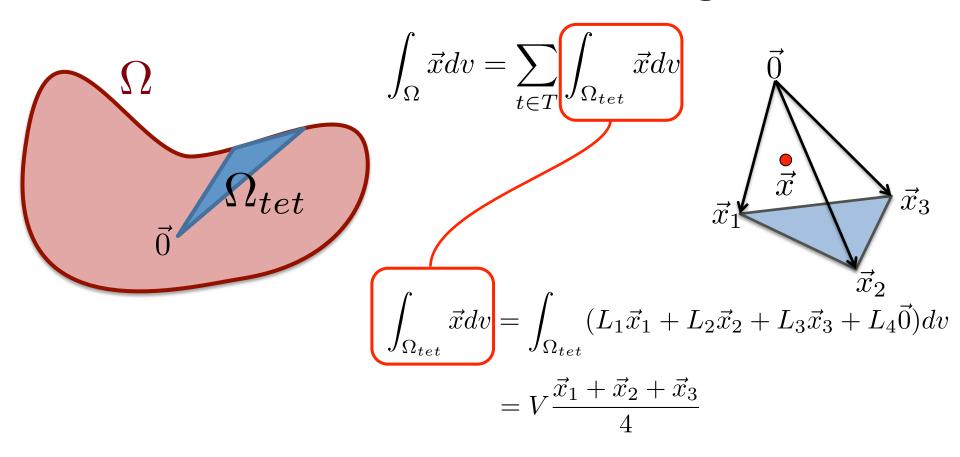
Roly-poly toy



Center of Mass for Shell Triangle Mesh



Center of Mass for Solid Triangle Mesh



Center of Mass for Solid Triangle Mesh II

The divergence theorem for tensor

$$\int_{\Omega} \vec{x} dv = \int_{\Omega} (\nabla \cdot \mathbf{T}) dv = \int_{\partial \Omega} (\mathbf{T} \cdot \vec{n}) ds$$

$$\nabla \cdot \mathbf{T} = \vec{x}$$
 What's the \mathbf{T} looks like?

Center of Mass for Solid Triangle Mesh II

The divergence theorem for tensor

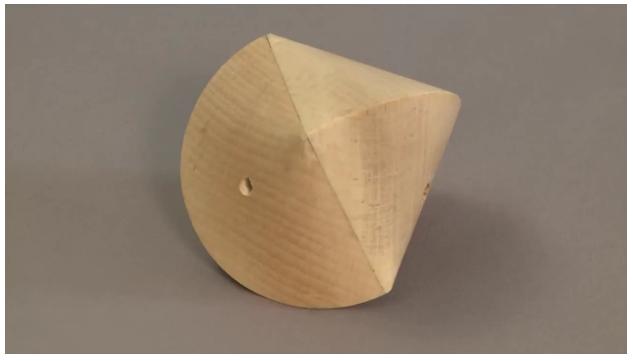
$$\int_{\Omega} \vec{x} dv = \int_{\Omega} (\nabla \cdot \mathbf{T}) dv = \int_{\partial \Omega} (\mathbf{T} \cdot \vec{n}) ds$$

$$\nabla \cdot \mathbf{T} = \vec{x}$$
 What's the \mathbf{T} looks like?

One example:
$$\mathbf{T} = \frac{1}{2} \begin{pmatrix} x^2 & 0 & 0 \\ 0 & y^2 & 0 \\ 0 & 0 & z^2 \end{pmatrix}$$

Interesting Object: Sphericon



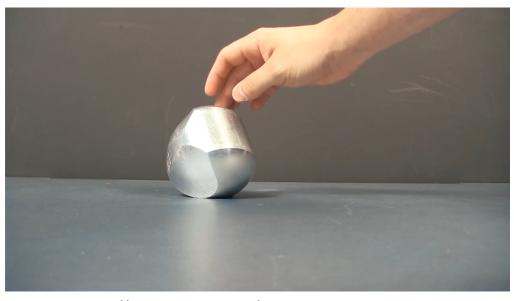


https://www.youtube.com/watch?v=L4KQmk7QEVQ

Interesting Object: Gomboc

Convex and homogeneous object that has a single stable configuration





https://www.youtube.com/watch?v=p96YazGhlY4

Research in CG: Make it Stand

Make It Stand: Balancing Shapes for 3D Fabrication

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Romain Prévost<sup>1</sup> Emily Whiting<sup>1</sup> Sylvain Lefebvre<sup>2</sup> Olga Sorkine-Hornung<sup>1</sup>

<sup>1</sup>ETH Zurich <sup>2</sup>INRIA
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(contains audio)

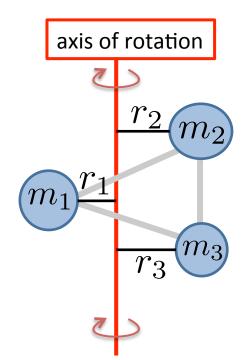
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The Moment of Inertia

We can define moment & energy of rotating object using MI

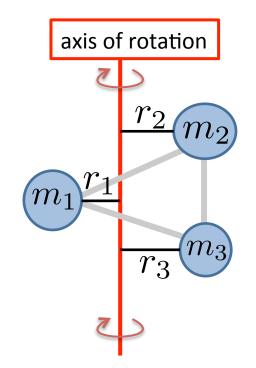
$$I = \sum m_i r_i^2$$



The Moment of Inertia

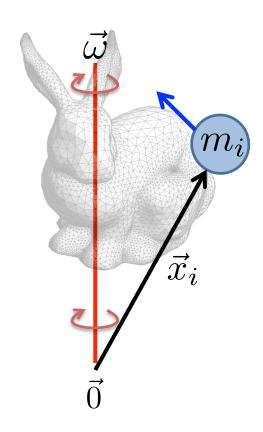
We can define moment & energy of rotating object using MI

$$I = \sum m_i r_i^2$$



$$I = \int_{\Omega} \rho(\vec{x}) r(\vec{x})^2 dv \xrightarrow{\text{Homogeneous}} I = \rho \int_{\Omega} r(\vec{x})^2 dv$$

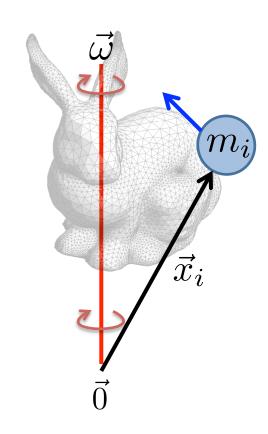
Angular Momentum and MI



angular momentum

$$\vec{L} = \sum \vec{x}_i \times (m_i \vec{v}_i)$$

Angular Momentum and MI

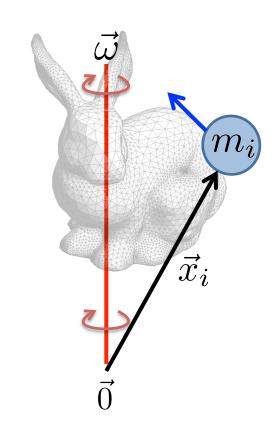


angular momentum

$$\vec{L} = \sum \vec{x}_i \times (m_i \vec{v}_i)$$

$$= \sum m_i \vec{x}_i \times (\vec{\omega} \times \vec{x}_i)$$

Angular Momentum and MI



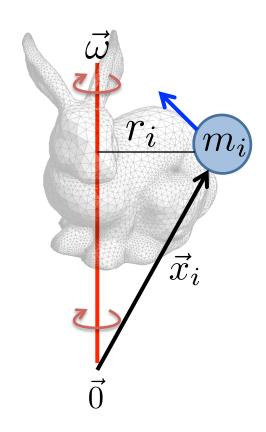
angular momentum

Conservation of Angular Momentum



https://www.youtube.com/watch?v=UZIW1a63KZs

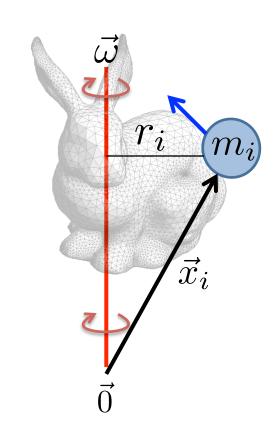
Kinetic Energy and MI



Kinetic Energy

$$E = \sum_{i=1}^{\infty} \frac{1}{2} m_i |\vec{v}_i|^2$$

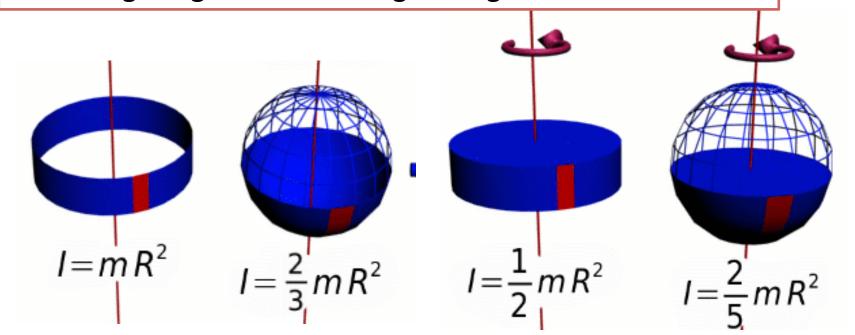
Kinetic Energy and MI



Kinetic Energy
$$E = \sum rac{1}{2} m_i |ec{v}_i|^2$$
 $= \sum rac{1}{2} m_i (|ec{w}| r_i)^2$ $= rac{1}{2} I |ec{\omega}|^2$

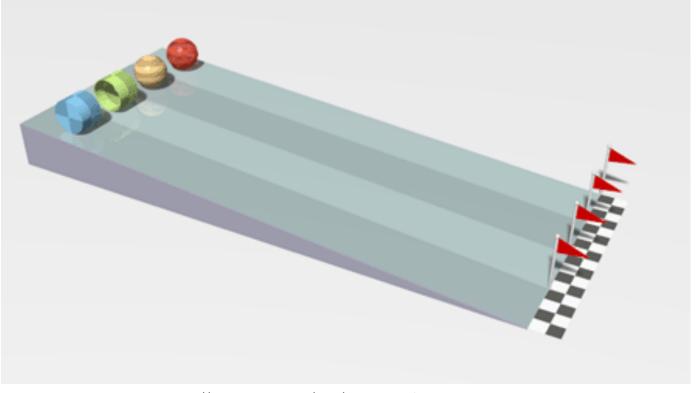
Example of Moment of Inertia

- Same weight give a different Moment of Inertia
- Putting weight outer ward give large Moment of Inertia



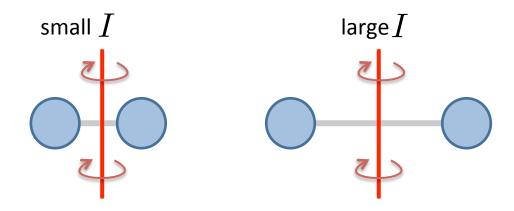
Slope Version of Galileo's Pisa Experiment





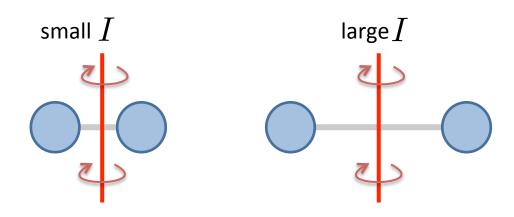
https://en.wikipedia.org/wiki/Moment_of_inertia

Application: Flywheel



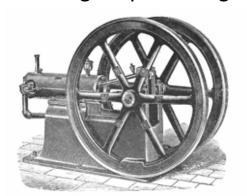


Application: Flywheel





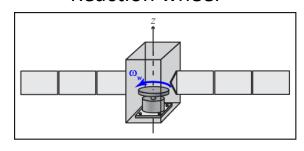
Smoothing output of engine

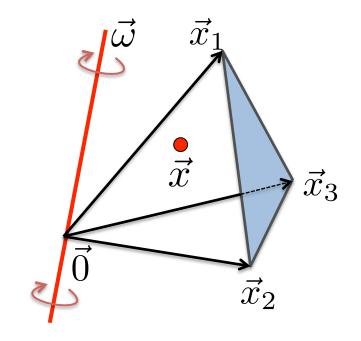


Energy storage



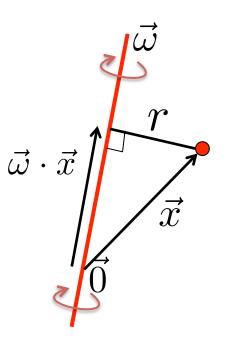
Reaction wheel





$$\vec{x} = L_1 \vec{x}_1 + L_2 \vec{x}_2 + L_3 \vec{x}_3 + L_4 \vec{0}$$

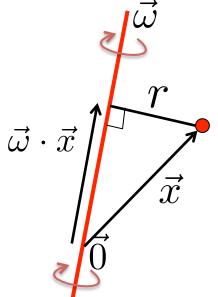
$$= L_i x_i$$



$$r^2 = (\vec{x} \cdot \vec{x}) - (\vec{\omega} \cdot \vec{x})^2$$

$$\vec{x} = L_1 \vec{x}_1 + L_2 \vec{x}_2 + L_3 \vec{x}_3 + L_4 \vec{0}$$

$$= L_i \vec{x}_i$$

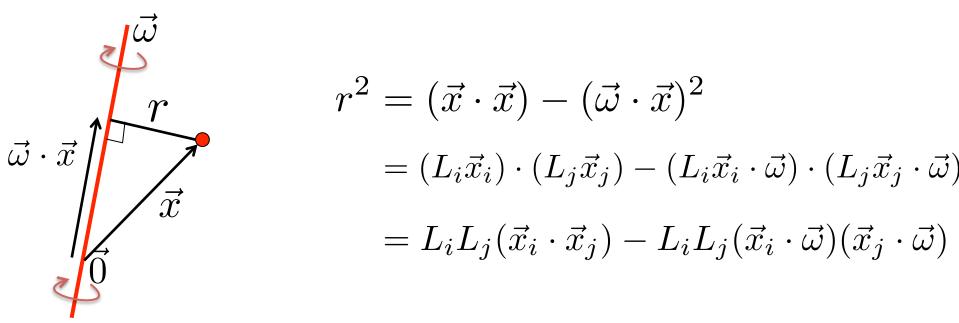


$$r^{2} = (\vec{x} \cdot \vec{x}) - (\vec{\omega} \cdot \vec{x})^{2}$$

$$= (L_{i}\vec{x}_{i}) \cdot (L_{j}\vec{x}_{j}) - (L_{i}\vec{x}_{i} \cdot \vec{\omega}) \cdot (L_{j}\vec{x}_{j} \cdot \vec{\omega})$$

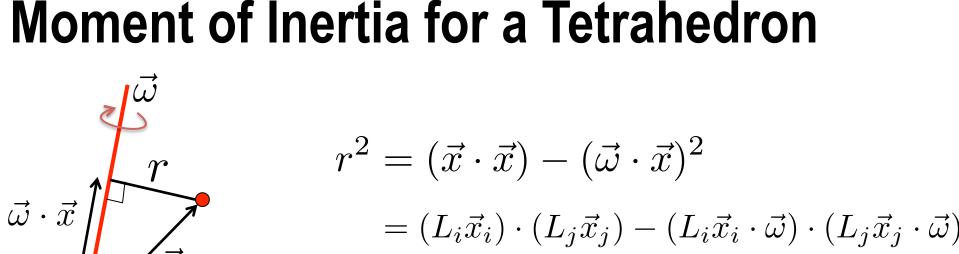
$$\vec{x} = L_1 \vec{x}_1 + L_2 \vec{x}_2 + L_3 \vec{x}_3 + L_4 \vec{0}$$

$$= L_i \vec{x}_i$$



$$\vec{x} = L_1 \vec{x}_1 + L_2 \vec{x}_2 + L_3 \vec{x}_3 + L_4 \vec{0}$$

$$= L_i \vec{x}_i$$



$$= (L_i \vec{x}_i) \cdot (L_j \vec{x}_j) - (L_i \vec{x}_i \cdot \vec{\omega}) \cdot (L_j \vec{x}_j \cdot \vec{\omega})$$

$$= L_i L_j (\vec{x}_i \cdot \vec{x}_j) - L_i L_j (\vec{x}_i \cdot \vec{\omega}) (\vec{x}_j \cdot \vec{\omega})$$
integration

$$\vec{x} = L_{i}L_{j}(\vec{x}_{i} \cdot \vec{x}_{j}) - L_{i}L_{j}(\vec{x}_{i} \cdot \vec{\omega})(\vec{x}_{j} \cdot \vec{\omega})$$

$$\vec{x} = L_{1}\vec{x}_{1} + L_{2}\vec{x}_{2} + L_{3}\vec{x}_{3} + L_{4}\vec{0}$$

$$= L_{i}\vec{x}_{i}$$

$$integration$$

$$\int_{V} L_{1}^{a}L_{2}^{b}L_{3}^{c}L_{4}^{d}dv = \frac{a!b!c!d!3!}{(a+b+c+d+3)!}V$$

$$\frac{V}{20}(i \neq j), \quad \frac{V}{10}(i = j)$$

Research in CG: Spin-It

Spin-It: Optimizing Moment of Inertia for Spinnable Objects

Moritz Bächer Disney Research Zurich **Emily Whiting** ETH Zurich

Bernd Bickel Disney Research Zurich

Olga Sorkine-Hornung **ETH Zurich**









Take aways

- Integration formula: divide region into simplexes
- Switch a volume/surface integration using the divergence theorem
- Three moments of shapes
 - mass, center of mass, moment of inertia
- Many physics are given by the moments
 - floating, standing, rotation